MIX DESIGN PROCEDURES

WMA Webinar September 18, 2013



Overview

- Present guidelines for design with WMA/RAP/RAS
- Identify WMA processes for various WMA technologies
- Identify differences in HMA/WMA mix design
- Discuss evolution of WMA mix design
- Review Best Practices



"Warm Mix" Definition

- A. Asphalt mixtures produced at temperatures approximately 50°F lower than for HMA?
- B. Technologies used as coating and compaction aids without reduction in temperature?
- C. Technologies that allow reduced temperature for producing, placing, and compacting asphalt mixtures?



- Organic Additives
- Chemical Additives
- Foaming Processes
- Hybrid Processes



Additive added to the binder





Additive added to the binder

Additive added to the mix





- Additive added to the binder
- Additive added to the mix
- Wet aggregate mix





- Additive added to the binder
- Additive added to the mix
- Wet aggregate mix
- Foamed mix





Adding WMA in Mix Design

- Drop-in HMA design
 - Risks
 - Less binder absorption
 - Less aging (May change binder properties, rutting)
 - Moisture susceptibility
- Separate mix design?
 - 2005 3 technologies
 - Now 30+



WMA Technologies

Advanced Concepts Engineering Co.: **LEA-CO**

AESCO/Madsen: Eco-Foam II Akzo Nobel: Rediset WMX All States Materials Group: ECOBIT Arkema Group: CECABASE RT Aspha-min: Aspha-min Online Astec Industries: Double Barrel Green System

Engineered Additives: **BituTech PER** Gencor Industries: **Green Machine** Herman Grant Company: **HGrant Warm Mix System**

Iterchimica: Qualitherm

Kumho Petrochemical and Korea Institute of Construction Technology:

LEADCAP

Maxam Equipment Inc.: Aquablack Warm Mix Asphalt McConnaughay Technologies: Low **Emission Asphalt** MeadWestvaco Asphalt Innovations: **Evotherm** Meeker Equipment Corp. Inc.: Meeker Warm Mix PQ Corporation: Advera WMA Sasol Wax North America Corporation: Sasobit Shell: Shell Thiopave Sonneborn Products: SonneWarmix Stansteel: Accu-Shear Dual Warm-Mix Additive System Tarmac Inc.: Tri-Mix Warm Mix Injection Terex Roadbuilding: Warm Mix Asphalt System



Differences in Design Procedure

- Only minor changes to AASHTO R35
 - Appendix 2
 - Specimen Fabrication
 - Coating & Compactibility for mixing and compaction temperatures
- Simulating plant foaming process
- Compactibility, stripping, & rutting may be different



Differences Needing More Research



- WMA mixing with bucket mixers
 - Less efficient, but more available
 - Coating as a function of mixing time



Planetary Mixers

- Used for NCHRP 9-43
- Mixing times used in AASHTO R35



Differences Needing More Research



Asphalt Foaming Devices

- Does lab foaming simulate field devices
- Is all foam equal
- How long is foam effective?



Differences Needing More Research

- STOA for moisture susceptibility & rutting resistance
 - HMA=4 hours @ 275F
 - WMA=2 hours @ compaction temp
 - Two-step conditioning



National Research Initiatives

NCHRP 9-43, Mix Design Practices for Warm Mix Asphalt



HIGHWAY RESEARCH PROGRAM

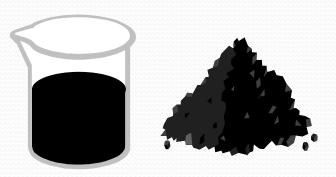
NATIONAL COOPERATIVE

Mix Design Practices for Warm Mix Asphalt

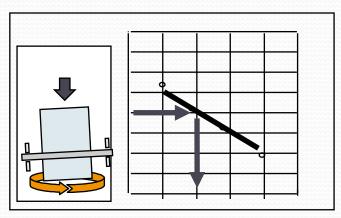
TRANSPORTATION RESEARCH BOARD



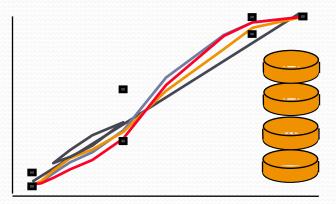
4 Steps in Mix Design



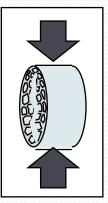
1. Materials Selection



3. Design Binder Content



2. Design Aggregate Structure



4. Performance Testing



Materials Selection

1. Select the process to be used



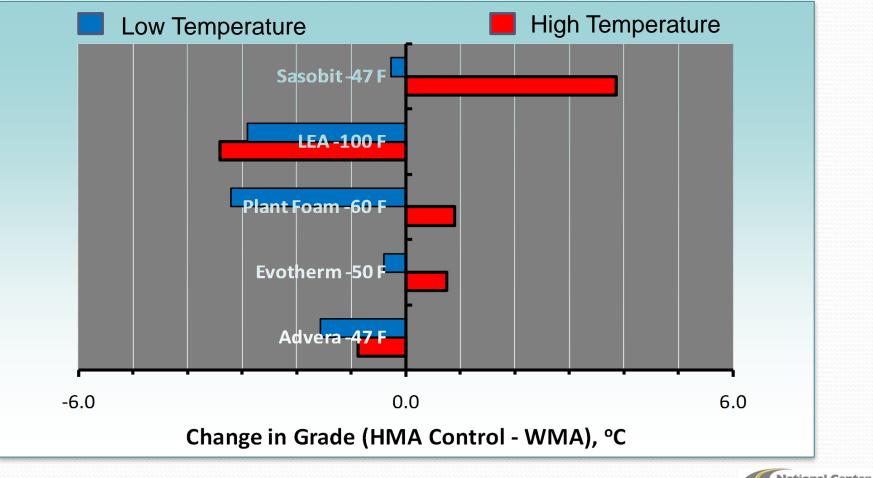
2. Binder Selection

Use same grade normally used for HMA *

* If WMA is 100°F lower than HMA, increase high temperature one grade.



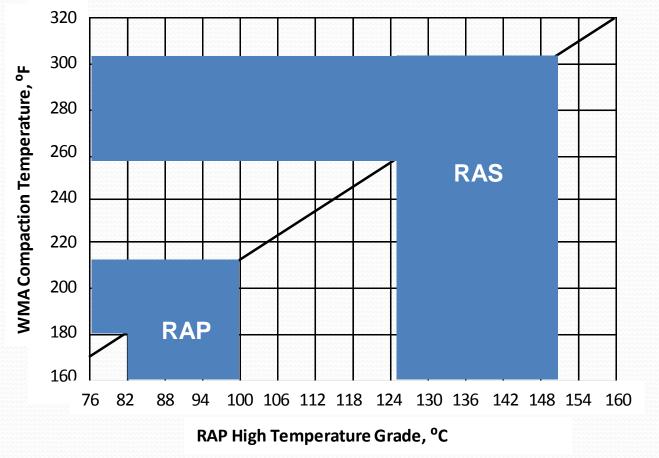
Effect of Technology on Binder Grade





RAP & RAS in WMA

Criteria: High grade of RAP/RAS must be ≤ planned field compaction temperature





How much RAP can I use?

- Anticipated optimum asphalt content = 5.5%
- RAP has 5.0% asphalt
- RAP low temp grade = -17.5°C
- Virgin AC low temp grade = -23.8°C
- Desired blend low temp grade = -22°C
- Assume WMA technology reduces low temp by 2°C



% Rap Binder (of Blend)

• % RAP Binder (of blend) =
$$\left(\frac{T_{blend} - T_{virgin}}{T_{RAP} - T_{virgin}}\right) \times 100$$

$$= \left(\frac{-22 - (-23.8)}{-17.5 - (-23.8)}\right) \times 100$$

$$=\frac{1.8}{6.3} \times 100 = 28.6\%$$

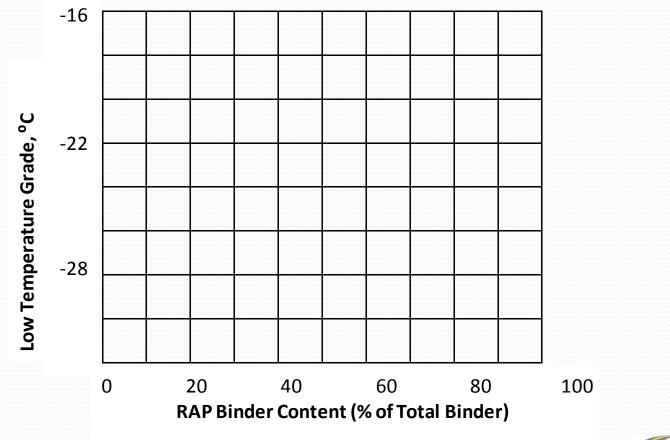


Maximum % RAP

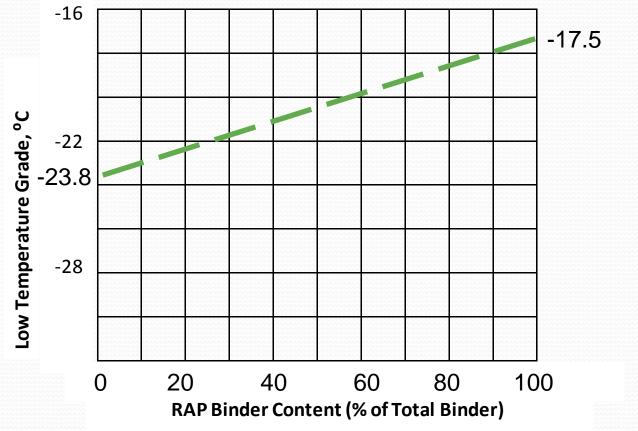
• Max. % RAP = $100 \times \frac{\% RAP \text{ binder of Blend} \times \% \text{ Total AC}}{\% \text{ binder in RAP}}$

 $= 100 \times \frac{28.6\% \times 5.5\%}{5.0\%} = 31.5\% \text{ RAP}$

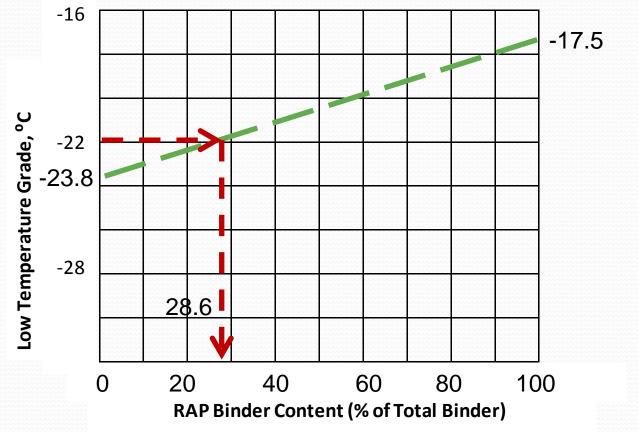




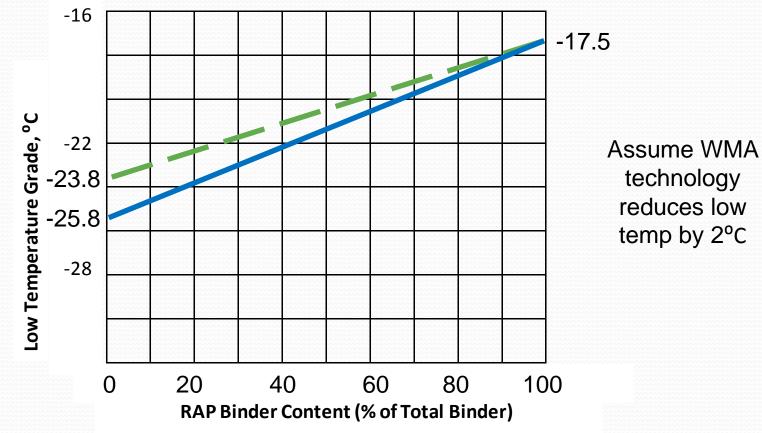
Asphalt Technology



Asphalt Technology NCAT at AUBURN UNIVERSITY



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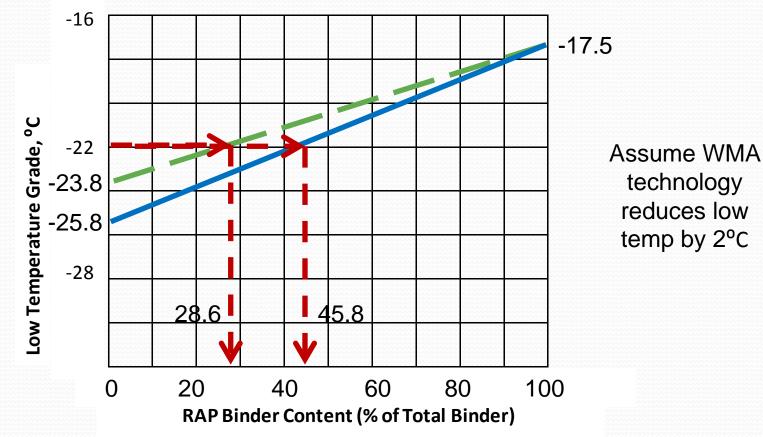
% Rap Binder (of Blend)

• % RAP Binder (of blend) =
$$\left(\frac{T_{blend} - T_{virgin}}{T_{RAP} - T_{virgin}}\right) \times 100$$

$$= \left(\frac{-22 - (-25.8)}{-17.5 - (-25.8)}\right) \times 100$$

$$=\frac{3.8}{8.3} \times 100 = 45.8\%$$





Asphalt Technology NCAT at AUBURN UNIVERSITY

Maximum % RAP

• Max. % RAP = $100 \times \frac{\% RAP \text{ binder of Blend} \times \% \text{ Total AC}}{\% \text{ binder in RAP}}$

 $= 100 \times \frac{45.8\% \times 5.5\%}{5.0\%} = 50.4\% \text{ RAP}$



RAP in WMA

- Planned field compaction temp > recovered high temp grade of RAP binder
- Some agencies assume < 100% blending
 - Example 1: 100% blending with 5.5% Total AC
 - RAP AC = 28.6% of total AC
 - 5.5% × 28.6% = 1.57% AC from RAP; 3.93% new AC
 - Example 2: 75% blending with 5.5% Total AC
 - 5.5% × 28.6% × 75%= 1.18% AC from RAP; 4.32% new AC



Number of Specimens

| Specimen Type | Size | Approx. Mass | Number Required |
|----------------------------|--|----------------------------------|---|
| G _{mm} | N/A | 500-6,000 g (depends on NMAS) | 2 per trial, 8 for design, 1 for compactibility |
| Volumetrics | 150 mm diam <mark>eter ×</mark> 115 mm high | 4,700 g | 2 per trial, 8 for mix design |
| Coating | N/A | 500-6,000 g (depends on NMAS) | 1 at optimum |
| Compactibility | 150 mm diameter × 115 mm high | 4,700 g | 4 at optimum |
| Moisture Susceptibility | 150 mm diameter × 95 mm high | 3,800 g | 6 at optimum |
| Flow Number | 150 mm diameter × 175 mm high | 7,000 g | 4 at optimum |



Temperatures

- Aggregate 15°C higher than planned production temperature
- RAP- heat with aggregate; limit to 2 hours
- Binder- heat to planned production temperature
- Short-term conditioning- heat 2 hours at planned compaction temperature



WMA Additives Added to Binder



- Weigh required additive (by wt. of binder) into small container
- Heat covered binder in 135°C oven until able to pour
- Add additive to binder and stir
- Store in covered container at room temperature until ready to use



WMA Additives Added to Binder



- Prepare Specimens:
 - Heat to previous mentioned temp
 - Add liquid anti-strip to binder (if required)
 - Dry mix hot aggregate and RAP
 - Form crater and add binder
 - Mix 90 seconds
 - 2 hour aging at planned field compaction temp



WMA Additives Added to Mixture

- Weigh required additive into small container
 - Based on Total AC, or Total mix?
- Add liquid anti-strip to binder (if required)
- Dry mix hot aggregate and RAP
- Form crater and add binder
- Pour WMA additive into pool of new binder
- Mix 90 seconds
- 2 hour aging At planned field compaction temp



WMA with Wet Aggregate Fraction

- Weigh required additive into small container
 - By weight of binder
- Heat covered binder in 135°C oven until able to pour
- Add additive to binder and stir
- Add moisture to wet aggregate fraction; mix, cover and let stand for 2 hours



WMA with Wet Aggregate Fraction

- Prepare Specimens:
 - Dry mix hot dry aggregate portion and RAP
 - Add additive to binder immediately before mixing
 - Form crater and add binder
 - Mix 30 seconds
 - Add wet aggregate fraction; mix for 60 more seconds
 - Mix shall be between 90-100°C (194-212°F)
 - 2 hour aging at planned field compaction temp



WMA Foamed Mixtures

- Add liquid anti-strip additive to binder, if required
- Prepare foamed binder per supplier's instructions
- Dry mix hot aggregate and RAP
- Form crater and add foamed binder
- Mix 90 seconds
- 2 hour aging at planned field compaction temp



Mixture Coating

- Mixing Times in AASHTO R35
- Separate Coarse Aggregate
 - ≥ 12.5mm NMAS, use 9.5 mm sieve
 - ≤ 9.5 mm NMAS, use 4.75 mm sieve
 - Minimum of 200 particles
- Evaluate per AASHTO T195
- Criteria: ≥ 95%

% Coated Particles =
$$\left(\frac{No. of fully coated particles}{No. of total particles}\right) \times 100$$



Compactibility

- Compact 2 specimens @ optimum AC to N_d at planned field compaction temperature
 - Determine gyrations to 92% of G_{mm}
- Compact 2 specimens @ optimum AC to N_d at 30 °C below planned field compaction temperature
 - Determine gyrations to 92% of G_{mm}
- Criteria: Ratio ≤ 1.25

Ratio =
$$\frac{(N_{92})T - 30}{(N_{92})T} \le 1.25$$



Calculate % G_{MM} for Each Gyration

% $G_{mm} = 100 \times \left(\frac{G_{mb} \times hd}{G_{mm} \times hn}\right)$



Compactibility

Gmm = 2.572

Gmb = 2.469

| | Height, mm (T-30°C) | | | |
|-----------|---------------------|-------------|---------|-------|
| Gyrations | Specimen #1 | Specimen #2 | Average | % Gmm |
| : | : | : | : | : |
| 22 | 116.7 | 116.8 | 116.8 | 91.7 |
| 23 | 116.6 | 116.6 | 116.6 | 91.8 |
| 24 | 116.4 | 116.5 | 116.4 | 91.9 |
| 25 | 116.2 | 116.2 | 116.2 | 92.1 |
| 26 | 116.0 | 116.0 | 116.0 | 92.3 |
| • | • | : | • | • |
| 100 | 111.4 | 111.6 | 111.5 | 96 |

92% Gmm at 250°F (121°C) = 21 gyrations 92% Gmm at 196°F (91°C) = 25 gyrations Ratio = $\frac{25}{21}$ = 1.19, \leq 1.25



Compactibility

- If recovered RAP binder grade = PG 82-xx
 - Minimum compaction temperature = 82°C (180°F)



Moisture Susceptibility

- WMA with anti-strip: TSR \geq HMA in 67% of mixes
- WMA without anti-strip: TSR ≤ HMA in 79% of mixes
- Compact to 7.0 <u>+</u> 0.5% Va
- TSR <u>></u> 0.80
- No visual stripping



Flow Number

Test Conditions from AASHTO TP 79

- Compact prepared samples after 2 hour short-term conditioning at compaction temp
- Core 100 mm diameter by 150 mm high sample from 150 mm diameter by 175 mm high sample (AASHTO PP60)



Flow Number

Test Conditions from NCHRP 9-33

- Va = 7.0 ± 0.5%
- Temperature = 50% Reliability @ high pavement temperature per LTPPBind v 3.1
 - Surface = 20 mm depth
 - Other layers = Top of layer
 - No adjustments for traffic or speed
- Unconfined
- 600 kPa Repeated Deviator Stress
- 30 kPa Contact Deviator Stress



| Rutting Resistance AASHTO T 79, Flow Number | | | | |
|--|-------------------------|--|--|--|
| Traffic Level, Million ESALs | Flow Number, Minimum | | | |
| < 3 | N/A | | | |
| 3 to < 10 | 30 | | | |
| 10 to < 30 | 105 | | | |
| ≥ 30 | 415 | | | |



Consult WMA Technology Supplier for issues with:

- Coating
- Compactibility
- Moisture Sensitivity



Rutting Resistance:

Change binder grade (+1 high grade = factor of 2)



- Change binder grade (+1 high grade = factor of 2)
- Add RAP (25-30% RAP = +1 high grade)



- Change binder grade (+1 high grade = factor of 2)
- Add RAP (25-30% RAP = +1 high grade)
- Increase filler content (+ 50 fineness modulus = factor of 2)



- Change binder grade (+1 high grade = factor of 2)
- Add RAP (25-30% RAP = +1 high grade)
- Increase filler content (+ 50 fineness modulus = factor of 2)
- Decrease VMA (-1% = factor of 1.2)



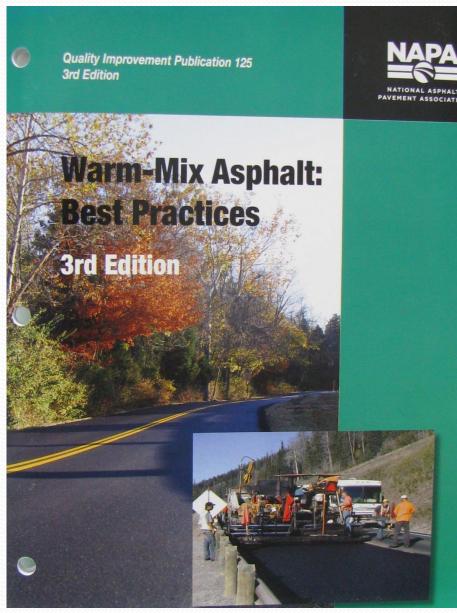
- Change binder grade (+1 high grade = factor of 2)
- Add RAP (25-30% RAP = +1 high grade)
- Increase filler content (+ 50 fineness modulus = factor of 2)
- Decrease VMA (-1% = factor of 1.2)
- Increase N_d (+1 level = factor of 1.2)



Summary

- Check WMA mixes for:
 - Coating
 - Compactibility
 - Moisture Sensitivity
 - Rutting Resistance
- Be sure whether additive rate based on binder weight or total mix weight



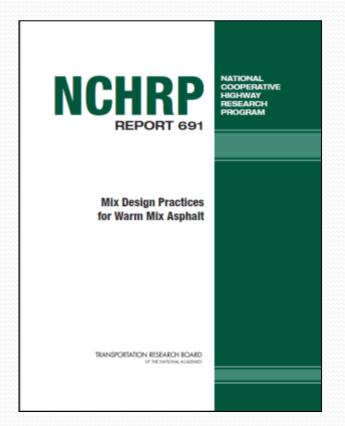


Available Resource



National Research Initiatives

- NCHRP 9-43 "Mix Design Practices for Warm Mix Asphalt"
- NCHRP Report 691
- Appendix to AASHTO R35





Course Number: FHWA-NHI-131137

Special Mixture Design Considerations and Methods for Warm Mix Asphalt - WEB-BASED

 PROGRAM AREA:
 Pavements and Materials

 COURSE NUMBER:
 FHWA-NHI-131137

 CALENDAR YEAR
 LENGTH
 CEU
 FEE

 2011
 2 Hours
 0 Units
 \$0 Per Participant

 2012
 2 Hours
 0 Units
 \$0 Per Participant

TRAINING LEVEL: Basic

CLASS SIZE: Minimum:1; Maximum:1

DESCRIPTION:

Highway transportation agencies are exploring the use of warm mix asphalt (WMA) for pavement projects. One of their main questions, particularly for agency mixture design technicians and engineers, is how WMA design differs from hot mix asphalt (HMA) design. "Mixture Design for Warm Mix Asphalt" is a Web-based training that presents the modifications to the current Superpave volumetric design procedure, as described in AASHTO R35, that are needed to complete a WMA mixture design. The training highlights key differences in WMA and HMA design procedures, and provides an opportunity to apply the AASHTO R35 standard practice to a WMA design modification.

Courtesy: Matt Corrigan, FHWA







